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Principal Investigators

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UNIVERSITY OF WASHINGTON

College of Engineering

Department of Electrical Engineering

Seattle, Washington 98195



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Annual Report for the Period Ending May 34, 19677

OPTICAL FIBER CUTTING MACHINE

FOR RECTANGULAR AND CIRCULAR FIBERS

Gordon L. Mitchell

June 20; 1977

Principal Investigators

Gordon L. Mitchell

and

William D. Scott

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Fiber Fracture Splicing Optical Controlled Fracture

30. ABSTRACT (Continue on reverse side if necessary and identify by block number)

An optical fiber cutting machine for use with rectangular or round cross section fibers has been developed. It combines a cliding-weight tension apparatus with a diamond knife crack initiation mechanism.

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Abstract

An optical fiber cutting machine for use with rectangular or round cross section fibers has been developed. It combines a sliding-weight tension apparatus with a diamond knife crack initiation mechanism.

Efficient butt joints in optical fiber systems require that fiber ends be well finished. Since Gloge published a controlled fracture fiber finishing machine a number of variations have evolved. The fiber cutting machine described in this report was designed with the following objectives:

- · Capability to cut round or rectangular cross section fibers
- Convenient and reproducible adjustment of fiber tension and bending radius
- Maximum use of purchased (rather than locally fabricated) material to minimize cost.
- · Simple operating procedures

The resulting fiber cutting machine is shown in Figure 1. After setting fiber tension weights with a dynamometer the fiber is clamped in the movable block and then in the fixed block. When the support slide is pulled from under the moveable block a preset tension is applied to the fiber. Fiber breakage occurs when the diamond knife is lowered to contact the fiber.

Adjustment of fiber radius and tension for clean fiber fractures is accomplished by trial and error. With the machine shown in Figure 1, a 125 µm diameter glass fiber required 300 grams tension and a 1.5" radius block for best breaks. The fiber tension can be reset within 5 grams of a desired value by positioning the sliding weights as shown in Figure 2. A tension vs. weight position calibration should be plotted for each fiber cutter constructed

REFERENCE

D. Gloge, P. W. Smith, D. L. Bisbee, E. L. Chinnock, Bell Syst. Tech. J. 52, pp. 1579-1588, (Nov. 1973).

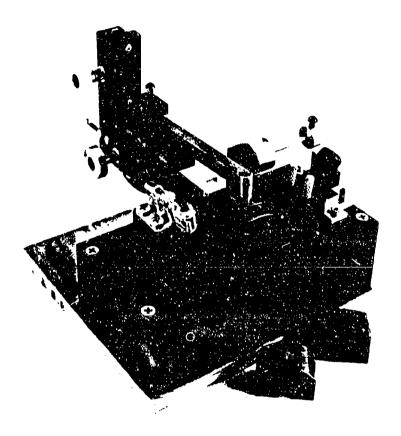


Figure 1 Fiber cutting machine. The fiber is held under tension over the radius block. When it is touched by the diamond knife a crack propagates across the fiber. If tension and radius are correct this will produce an optical quality end finish.

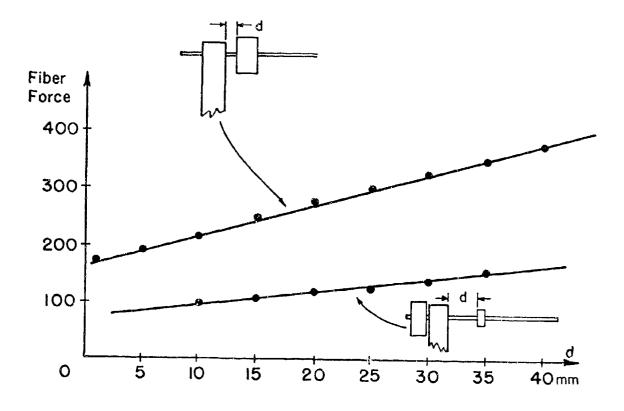


Figure 2. Fiber tension as a function of weight position for a prototype machine shown in Figure 1.

ACKNOWLEDGEMENT

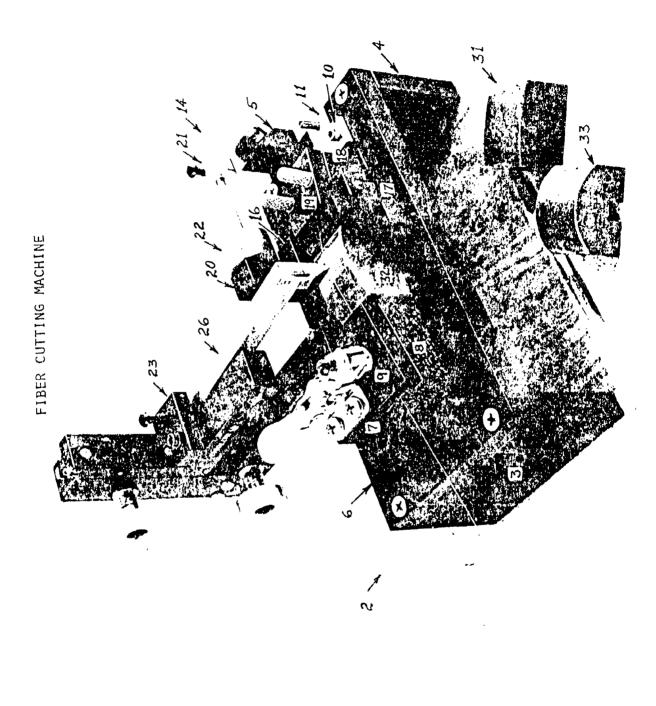
The fiber cutter described in this report uses some design concepts from similar machines constructed at Bell Telephone Laboratories and the Naval Ocean Systems Center. Marcell Sollenberger fabricated the first prototypes and David Porter of the Boeing Commercial Airplane Company was responsible for design documentation.

DETAIL DRAWINGS

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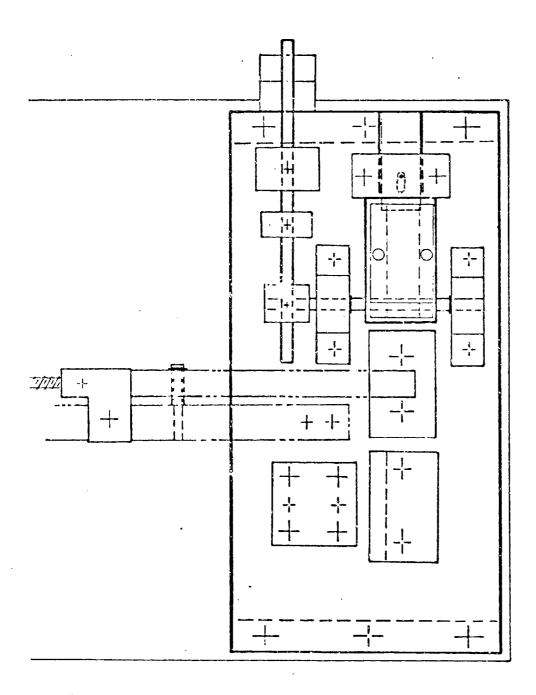


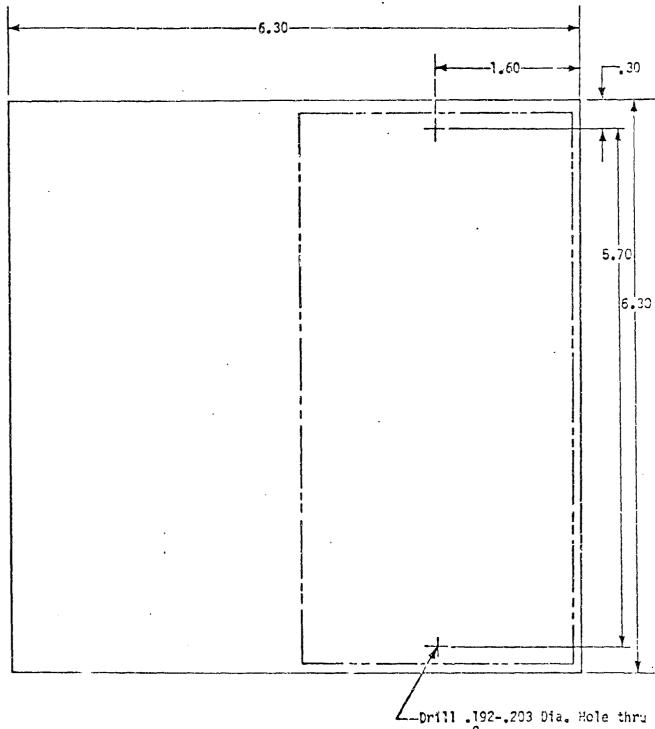
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		1	MS171431	PIN	SPRING		
		1	MS171525	PIN	SPRING	ĺ	ļ
		1	NAS1189-08-4	SCREW	FLAT HEAD		
		6	NAS1189-08-12	SCREW	FLAT HEAD		
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			Al uminum	Alloy; 6061-T4			
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			~8-	REV LTR	
-3	30 1	-26	cutter arm rework	Bell Labs Diamond Knife Victory Diamond Tool Co. P. O. Box 274 East Hanover, N.J. 07936	
-2	26 1	-27	balance screw	6-32 UNCx2.50 LONG	
-2	26 1	-28	cutter arm weight	.45 DIAx.48 LONG ST. STEEL	
-	1 1	-30	mechanical stage MA88	Swift Mechanical Stage College Biological Supply 21707 Bothell Way Bothell, Washington 481-0731	
-	1 1	-31	3" radius block	1.20x.85x.74 Al. Alloy	
_	1 1	-32	1.5" radius block	1.20x.85x.74 Al. Alloy	
-	1 1	-33	.75" radius block	1.20x.85x.74 Al. Alloy	
-	1 1	2059	toggle clamp	De Sta Co Campbell Industrial Supply 3433 Airport Way So. Seattle, Washington 98134 447-7100	
	12 2 30 1	-	CIRCLIP	1/8" DIAMETER	
-	5 1	-	GROMMET	.60" DIA, RUBBER	Ì
-2	21 1	4-40	SCREW	SLOT HEAD, TEFLON	Ì
-2	22 1	6-32	SCREW	SLOT HEAD, TEFLON	ļ
-2	26 1	6-32	SCREW	FLAT HEAD, 2.5 LONG	
-1	12 2	Ms 24585C29	SPRING		
	1	MS24677-1	SCREW	SOCKET HEAD	
	2	MS24677-7	SCREW	SOCKET HEAD	
	6	MS24677-10	SCREW .	SOCKET HEAD	
	1	MS24677-14	SCREW	SOCKET HEAD	
	2	MS24677-17	SCREW	SOCKET HEAD	
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7-	1	- 1	optical fiber cutt	er	
- 1	1	- 2	base beams	6.5 x 6.5 x 3/8 plywood	
- 1	1	- 3	end support	3.0x1.5x.36 Al. Alloy	
- 1	1	- 4	end support with restraint	3.0x1.5x.36 Al. Alloy	
- 1	1	- 5	restraint	1.75x.75x.60 Al. Alloy	}
- 1	1	- ő	mounting plate	6.06x3.0x.36 Al. Alloy	
- 1	1	- 7	clamp base	.96x.94x.78 Al. Alloy	ł
- 1	i	- 8	fiber restraint ba	se 1.24x.76x.74 Al. Alloy	
- 1	1	- 9	fiber restraint	1.24x.76x.25 Al. Alloy	
- 1	1	-10	slide plate retain	er 1.10x.50x.10 stainless steel	
- 1	1	-11	slide plate	1.12x.48x.10 stainless steel	
- 1	1	-12	tension clamp asse	mbly - ·	
-12	1	-14	lever bar	1/8"DIAx3.6 LONG stainless	
-12	1	-15	mounting bar	steel 1/8"DIAx2.45 stainless steel	
-12	1	-16	mounting bar suppo	rt 1.36x.35x.36 stainless steel	
-12	1	-17	bar end support	1.36x.85x.36 stainless steel	
-12	1	-18	tension clamp block	1.25x.75x.74 Al. Alloy	
-12	1	-19	tension clamp	1.10x.25x.74 Al. Alloy	
-12	1	-20	bar joint	1.10x.50x.42 A1. Alloy	
-12	1	-21	small weight	.56DIAx.28 LONG stainless	
-12	1	-22	large weight	steel .70DIAx.50 LONG stainless	
-30	1	-23	cutter arm block	steel 1.0x.80x.25 Al. Alloy	
-26	1	-24	bushing	bronze 1/8 I.D.x.35 LONG	
-30	1	-25	pivot pin	1/8 DIAx1.0 LONG stainless steel Rod	
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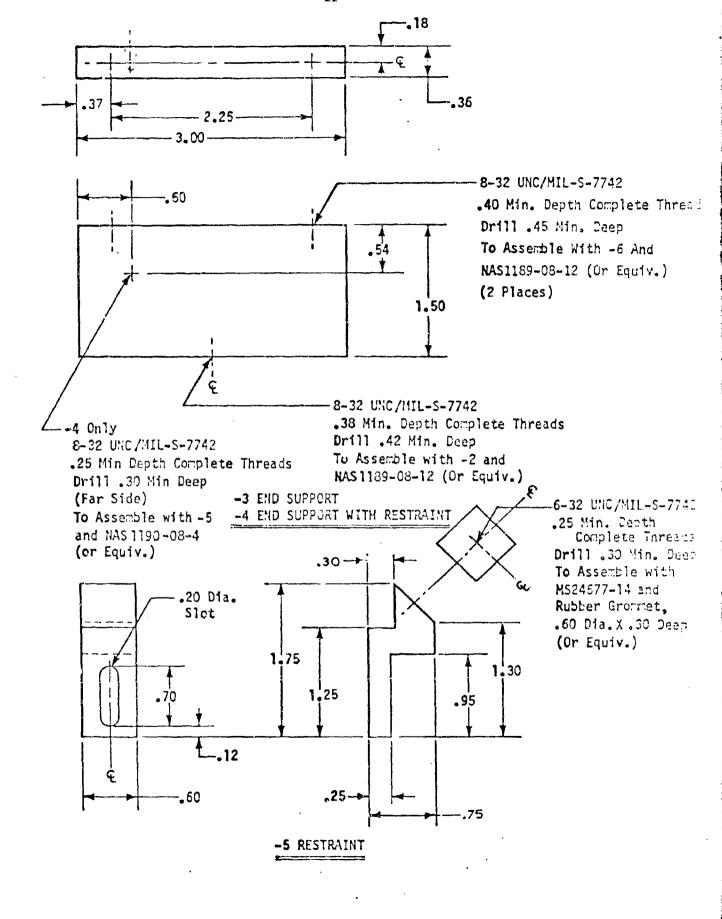


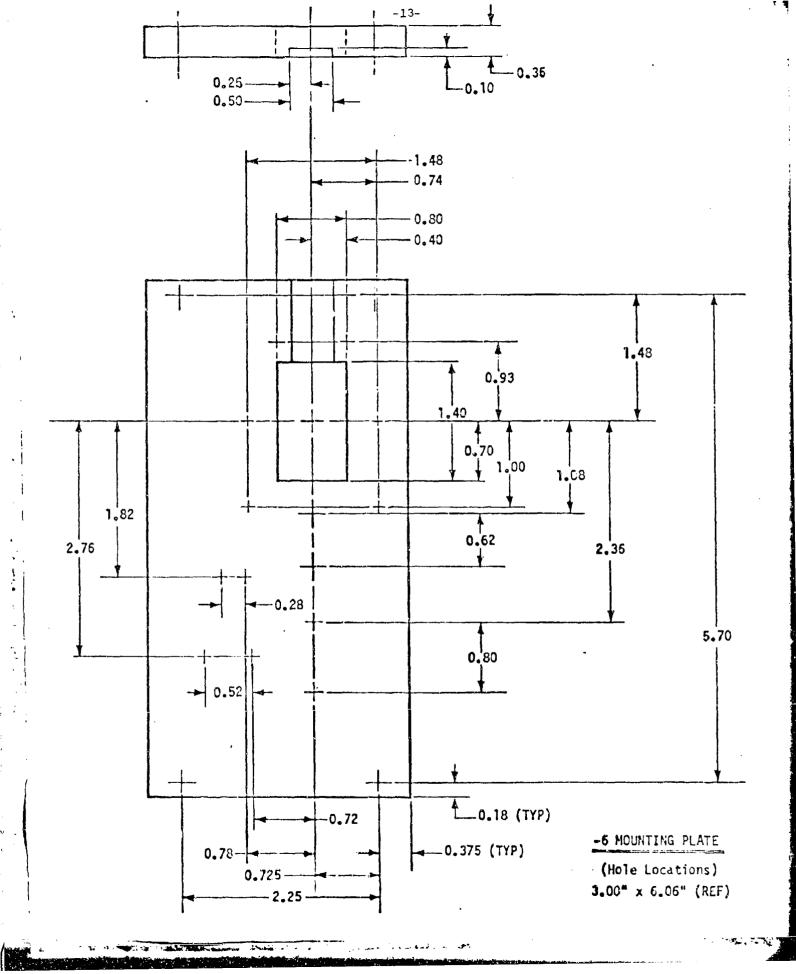


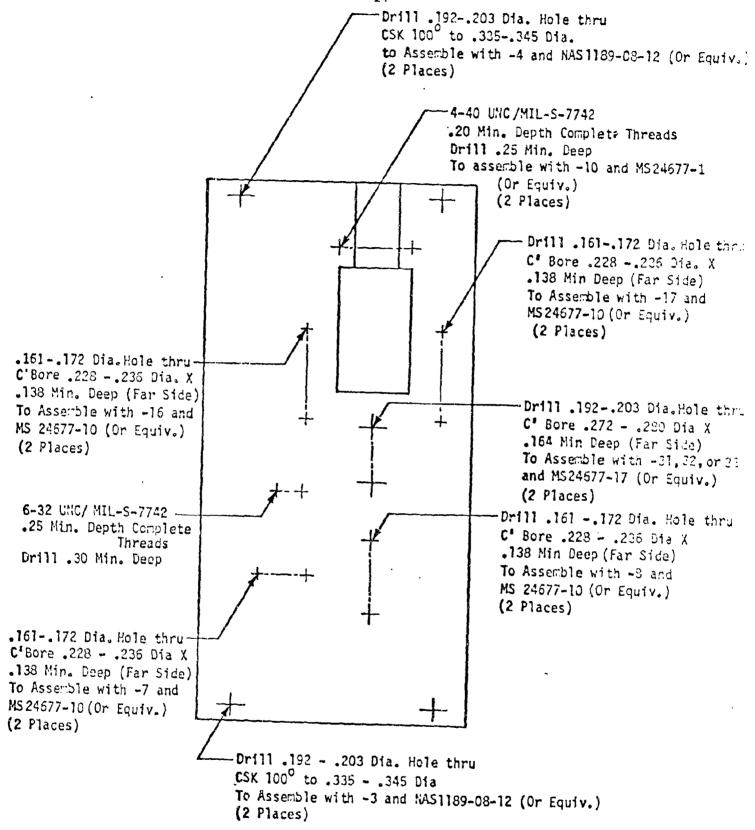
-Drill .192-.203 Dia. Hole thru CSK 100° to .335 - .345 Dia. to Assemble with -3 and -4. and NAS 1139-08-12 (or Equiv.) (2 Places)

<u>-2 BASE BOARD</u>

3/8 Plywood (Material Optional)







-6 MOUNTING PLATE
(FASTENERS)

-.52

6-32 UNC/MIL-S-7742

Complete Threads

Drill .45 Min. Deep

To Assemble with -6

.22 -

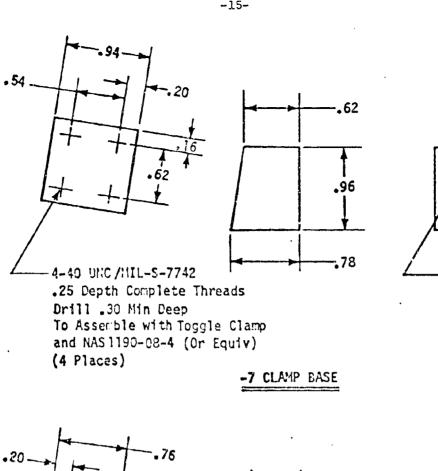
6-32 UNC/HIL-S-7742 .40 Min. Depth Complete Inreads Drill .45 Min. Deep To Assemble with -6 and MS24677-10 (Or Equiv.) (2 Places)

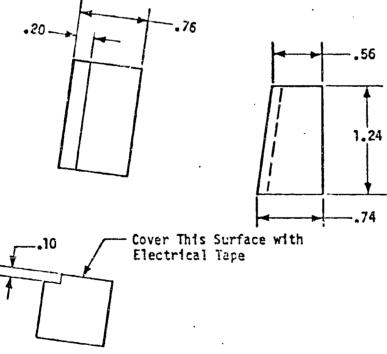
.40 Min. Depth

and MS24677-10

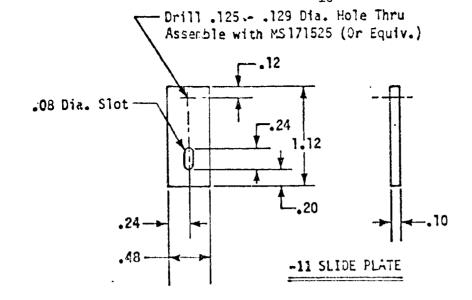
(Or Equiv.)

(2 Places)



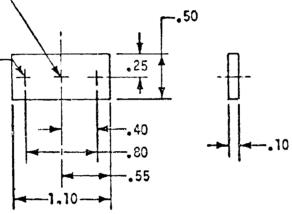


+8 FIBER RESTRAINT BASE

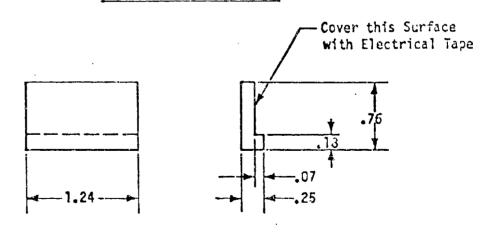


.062-.065 Dia. Hole thru
Assemble with MS171431
(Or Equiv.)

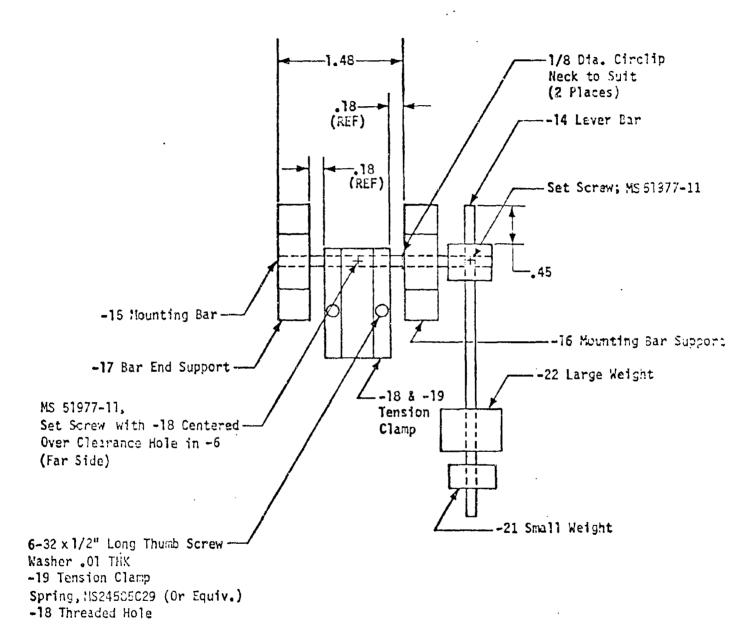
.135-.147 Dia.Hole thru-To Assemble with -6 and MS 24677-1 (Or Equiv.) (2 Places)



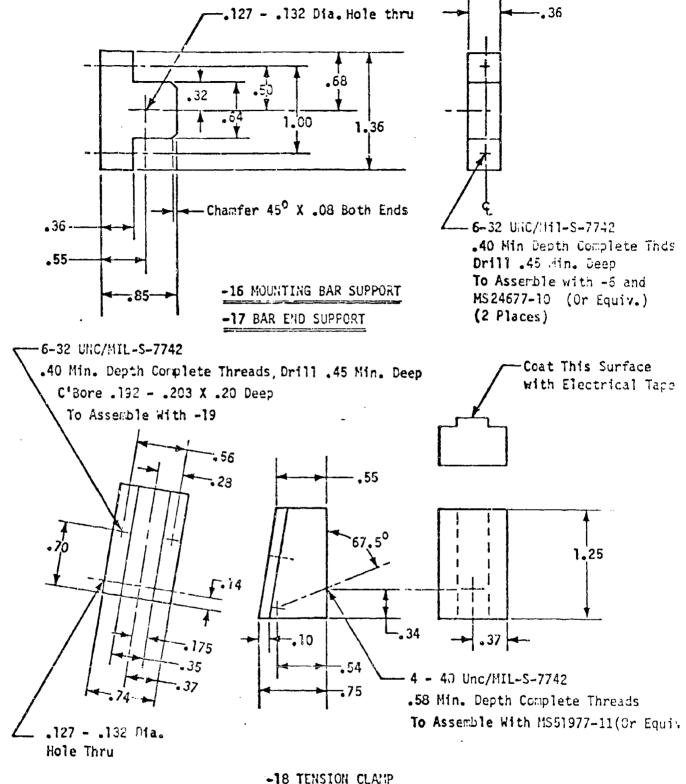
-10 SLIDE PLATE RETAINER



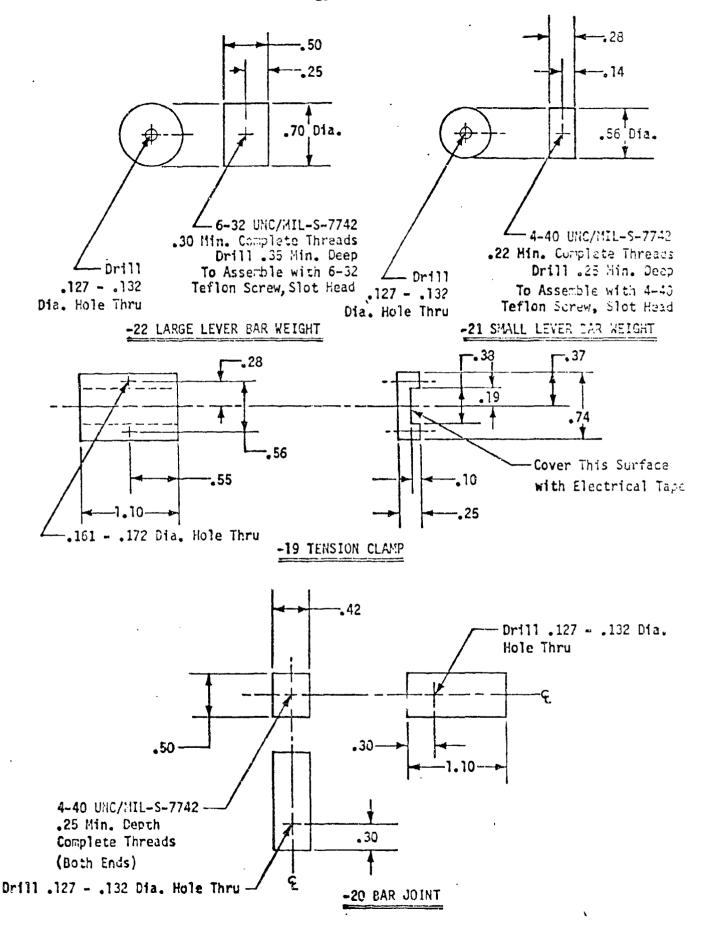
-9 FIBER RESTRAINT

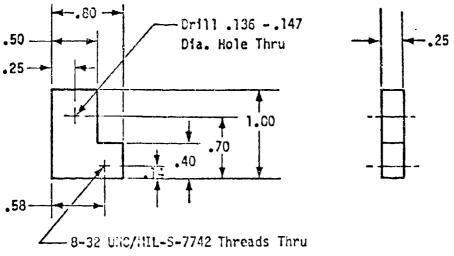


-12 TENSION CLAMP ASSEMBLY



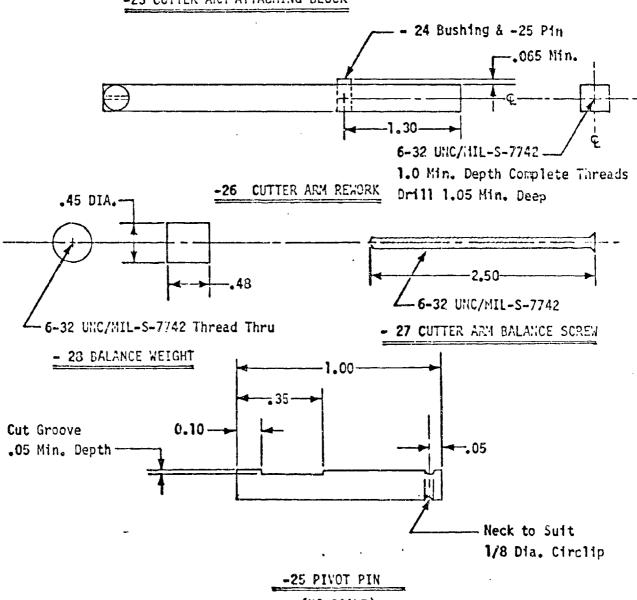
-18 TENSION CLAMP



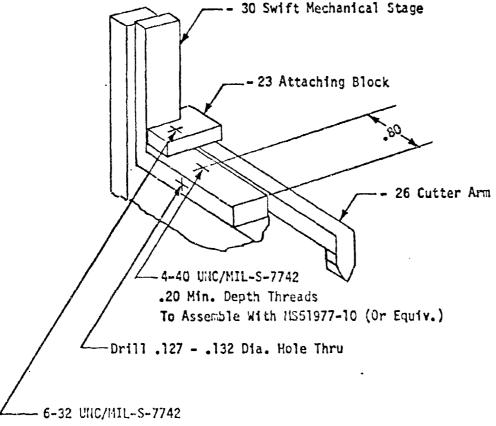


To Assemble With -30 and NAS1190-00-4 (Or Equiv.)

-23 CUTTER ARM ATTACHING BLOCK

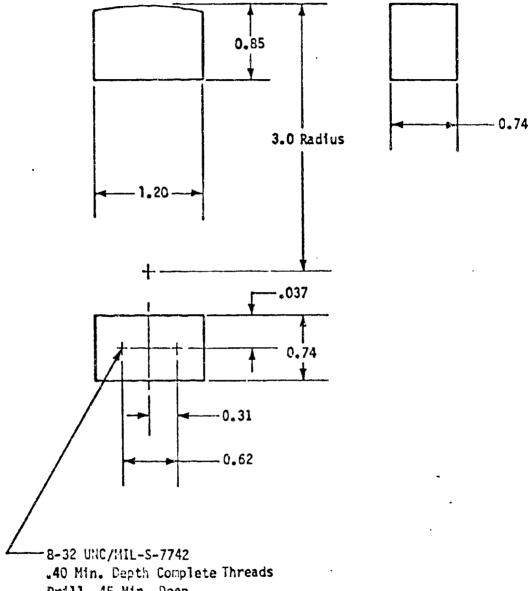


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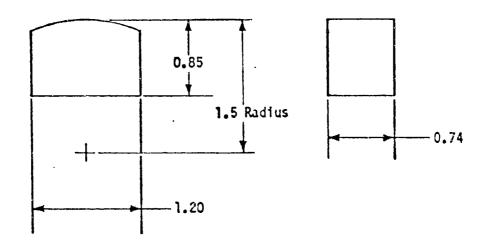
.30 Min. Depth Complete Threads
Drill .35 Min. Deep
To Assemble with -23 and MS 24677-7

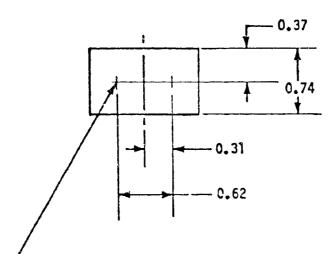
- 30 SWIFT MECHANICAL STAGE REWORK



.40 Min. Depth Complete Threads
Drill .45 Min. Deep
To Assemble with -6 and
MS 24677-17 (Or Equiv.)
(2 Places)

-31 BLOCK

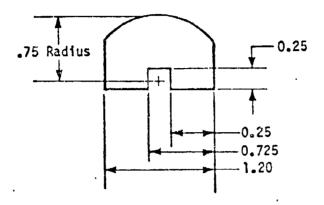


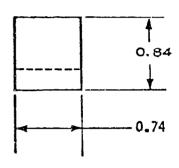


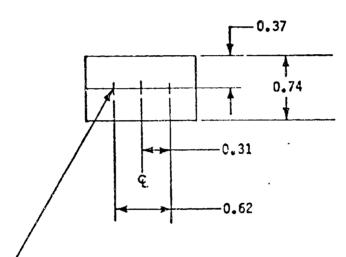
-8-32 UNC/MIL-S-7742

.40 Min. Depth Complete Threads
Drill .45 Min. Deep
To Assemble With -6 And
MS 24677-17 (Or Equiv.)
(2 Places)

- 32 BLOCK







8-32 UNC/MIL-S-7742
.40 Min. Depth Complete Threads
Drill .45 Min. Deep
To Assemble With -6 and
MS 24677-17 (Or Equiv.)
(2 Places)

-33 BLOCK